

BUREAU OF LOCAL ROADS AND STREETS MANUAL

## HARD COPIES UNCONTROLLED

## BUREAU OF LOCAL ROADS \& STREETS

## Chapter 30 <br> VERTICAL ALIGNMENT

## Table of Contents

Section Page
30-1 GRADES ..... 30-1-1
30-1.01 Terrain ..... 30-1-1
30-1.02 Maximum Grades ..... 30-1-1
30-1.03 Minimum Grades ..... 30-1-1
30-2 VERTICAL CURVE ..... 30-2-1
30-2.01 Crest Vertical Curves ..... 30-2-1
30-2.01(a) Basic Equations ..... 30-2-1
30-2.01(b) Curve Lengths ..... 30-2-1
30-2.02 Sag Vertical Curves ..... 30-2-6
30-2.02(a) Basic Equations ..... 30-2-6
30-2.02(b) Curve Lengths ..... 30-2-6
30-3 VERTICAL CLEARANCES ..... 30-3-1
30-4 ACRONYMS ..... 30-4-1
30-5 REFERENCES ..... 30-5-1

## Chapter 30

## VERTICAL ALIGNMENT

Chapter 30 presents Bureau of Local Roads and Streets (BLRS) criteria for the design of vertical alignment elements. This includes vertical curvature and grades for both crest and sag vertical curves.

## 30-1 GRADES

## 30-1.01 Terrain

The topography throughout most of Illinois is considered either level or rolling. However, the northwest corner of the State, southern Illinois, and bluff areas near major rivers may be considered rugged. In general, if the terrain designation is not clear (e.g., level versus rolling), select the flatter of the two terrains.

## 30-1.02 Maximum Grades

Figures 32-3A, 32-3B, and 32-3C in Chapter 32 present the maximum grade criteria based on functional classification, urban/rural location, type of terrain, and design speed. In addition, the designer should consider the following guidelines:

1. Grades should be as flat as is consistent with the surrounding terrain.
2. Only use maximum grades where absolutely necessary. Where practical, use grades flatter than the maximum.
3. Where grades of $4.0 \%$ or steeper are required, take special care to prevent erosion on slopes and open drainage facilities.

## 30-1.03 Minimum Grades

The following provides the criteria for minimum grades:

1. Uncurbed Roadways. It is desirable to provide a longitudinal grade of approximately $0.5 \%$. This allows for the possibility of alterations to the original pavement cross slope due to swell, consolidation, maintenance operations, or resurfacing. Longitudinal grades of $0.0 \%$ may be acceptable on some pavements that have adequate cross slopes. These locations typically occur where a highway traverses a wide flood plain. In these cases, check the flow lines of the outside ditches for adequate drainage.
2. Curbed Streets. The centerline profile of streets with curb and gutter should have a minimum longitudinal grade of $0.3 \%$; however, $0.5 \%$ is desirable. On curbed facilities,

## BUREAU OF LOCAL ROADS \& STREETS

the longitudinal grade at the gutter line will have a significant impact on the pavement drainage characteristics (e.g., water encroaching on travel lanes, flow capture rates by grates). See Chapter 38 of the BLRS Manual and the IDOT Drainage Manual for more information on pavement drainage.
3. New Bridges. For bridges on new construction and reconstruction projects, desirably provide a minimum longitudinal grade of $0.5 \%$ across the bridge for structures with curbed cross sections, in order to prevent ponding on the bridge.

## 30-2 VERTICAL CURVE

## 30-2.01 Crest Vertical Curves

## 30-2.01(a) Basic Equations

Crest vertical curves are in the shape of a parabola. The basic equations for determining the minimum length of a crest vertical curve are:

$$
\begin{align*}
& L=\frac{A S^{2}}{200\left(\sqrt{h_{1}}+\sqrt{h_{2}}\right)^{2}}  \tag{Equation30-2.1}\\
& L=K A
\end{align*}
$$

(Equation 30-2.2)
Where:
$\mathrm{L}=$ length of vertical curve, $\mathrm{ft}(\mathrm{m})$
A = algebraic difference between the two tangent grades, \%
$\mathrm{S}=$ sight distance, ft (m)
$\mathrm{h}_{1}=$ height of eye above road surface, $\mathrm{ft}(\mathrm{m})$
$\mathrm{h}_{2}=$ height of object above road surface, $\mathrm{ft}(\mathrm{m})$
$\mathrm{K}=$ horizontal distance needed to produce a $1.0 \%$ change in gradient, $\mathrm{ft} / \%$ ( $\mathrm{m} / \%$ )
The length of a crest vertical curve will depend upon "A" for the specific curve and upon the selected sight distance, height of eye, and height of object. The calculated value should be rounded to the next highest $10 \mathrm{ft}(10 \mathrm{~m})$ increment.

## 30-2.01(b) Curve Lengths

The following discusses the application of K-values:

1. Vertical Point of Intersection (PVI). For crest vertical curves, it is acceptable to use an angle point (i.e., no vertical curve) for an algebraic difference of grade ( $\Delta$ ) of $0.6 \%$ or less.
2. Stopping Sight Distance (SSD). The principal control in the design of crest vertical curves is to ensure that SSD is available throughout the vertical curve. Figures 30-2A and $30-2 \mathrm{~B}$ present the minimum K -values for passenger cars on a level grade by assuming $\mathrm{h}_{1}=3.5 \mathrm{ft}(1.080 \mathrm{~m})$, $\mathrm{h}_{2}=2 \mathrm{ft}(600 \mathrm{~mm})$, and $\mathrm{S}=\mathrm{SSD}$ in the basic equation for crest vertical curves (Equation 30-2.1). These values represent the lowest acceptable sight distance on a facility. Where cost effective, use higher than minimum stopping sight distances.

## BUREAU OF LOCAL ROADS \& STREETS

30-2-2

| US Customary |  |  |  | Metric |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Design Speed (mph) | $\begin{gathered} \operatorname{SSD}^{(1)} \\ (\mathrm{ft}) \end{gathered}$ | Rate of Vertical Curvature, $K^{(2)(3)}$ (ft/\%) | Minimum Curve Length (ft) | Design Speed (km/h) | $\begin{aligned} & \mathrm{SSD}^{(1)} \\ & (\mathrm{m}) \end{aligned}$ | Rate of Vertical Curvature, $\begin{aligned} & \mathrm{K}^{(2)(4)} \\ & (\mathrm{m} / \%) \end{aligned}$ | Minimum Curve Length (m) |
| 20 | 115 | 7 | 60 | 30 | 35 | 2 | 18 |
| 25 | 155 | 12 | 75 | 40 | 50 | 4 | 24 |
| 30 | 200 | 19 | 90 | 50 | 65 | 7 | 30 |
| 35 | 250 | 29 | 105 | 60 | 85 | 11 | 36 |
| 40 | 305 | 44 | 120 | 70 | 105 | 17 | 42 |
| 45 | 360 | 61 | 135 | 80 | 130 | 26 | 48 |
| 50 | 425 | 84 | 150 | 90 | 160 | 39 | 54 |
| 55 | 495 | 114 | 165 | 100 | 185 | 52 | 60 |
| 60 | 570 | 151 | 180 |  |  |  |  |

## Notes:

1. SSD values are from Figure 28-1A.
2. Maximum K-value for drainage on curbed roadways and bridges is 167 (51).
3. $K=\frac{S S D^{2}}{2158}$, where : $h_{1}=3.5 \mathrm{ft}, h_{2}=2 \mathrm{ft}$
4. $K=\frac{S S D^{2}}{658}$, where : $h_{1}=1.080 \mathrm{~m}, h_{2}=600 \mathrm{~mm}$

## K-VALUES FOR CREST VERTICAL CURVES — STOPPING SIGHT DISTANCES <br> (Passenger Cars)

Figure 30-2A


DESIGN CONTROLS FOR CREST VERTICAL CURVES
Figure 30-2B

## HARD COPIES UNCONTROLLED

3. Minimum Length. Vertical curve lengths should also meet the criteria in the following equations:
$L_{\text {min }}=3 \mathrm{~V}$
(US Customary) Equation 30-2.3
$L_{\text {min }}=0.6 \mathrm{~V}$
(Metric) Equation 30-2.3
Where:

$$
\begin{aligned}
\mathrm{L}_{\min } & =\text { minimum length of vertical curve, } \mathrm{ft}(\mathrm{~m}) \\
\mathrm{V} & =\text { design speed, } \mathrm{mph}(\mathrm{~km} / \mathrm{h})
\end{aligned}
$$

Designs with vertical curve lengths of less than $90 \mathrm{ft}(27 \mathrm{~m})$ should be avoided, since these are difficult to construct.
4. Passing Sight Distance (PSD). At some locations, it may be desirable to provide PSD in the design of crest vertical curves. Section 28-2 discusses the application and design values for PSD on two-lane, two-way highways. These "PSD" values are used in the basic equation for crest vertical curves (Equation 30-2.1). The height of eye $\left(\mathrm{h}_{1}\right)$ is 3.5 ft $(1.080 \mathrm{~m})$ and the height of object $\left(\mathrm{h}_{2}\right)$ is $3.5 \mathrm{ft}(1.080 \mathrm{~m})$. Figure $30-2 \mathrm{C}$ presents the Kvalues for passenger cars using the PSD presented in Section 28-2.
5. Drainage. Proper drainage should be considered in the design of crest vertical curves where curbed sections are used. Typically, drainage problems should not be experienced if the vertical curvature is sharp enough so that a minimum longitudinal grade of at least $0.3 \%$ is reached at a point about $50 \mathrm{ft}(15 \mathrm{~m})$ from either side of the apex. To ensure that this objective is achieved, determine the length of the crest vertical curve assuming a K-value of 167 (51) or less. For crest vertical curves on a curbed section where this K -value is exceeded, carefully evaluate the drainage design near the apex.
6. Alignment Coordination. On rural facilities where crest vertical curves and horizontal curves occur at the same location, use the K-values in Figure 30-2A to ensure that the horizontal curve is visible as drivers approach the vertical curve.

BUREAU OF LOCAL ROADS \& STREETS
August 2016

| US Customary |  |  | Metric |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Design Speed (mph) | PSD ${ }^{(1)}$ <br> (ft) | Rate of Vertical Curvature, $\mathrm{K}^{(2)}$ Design (ft/\%) | Design Speed (km/h) | $\begin{aligned} & \mathrm{PSD}^{(1)} \\ & (\mathrm{m}) \end{aligned}$ | Rate of Vertical Curvature, $\mathrm{K}^{(3)}$ Design $(\mathrm{m} / \%)$ |
| 20 | 710 | 180 | 30 | 200 | 46 |
| 25 | 900 | 289 | 40 | 270 | 84 |
| 30 | 1090 | 424 | 50 | 345 | 138 |
| 35 | 1280 | 585 | 60 | 410 | 195 |
| 40 | 1470 | 772 | 70 | 485 | 272 |
| 45 | 1625 | 943 | 80 | 540 | 338 |
| 50 | 1835 | 1203 | 90 | 615 | 438 |
| 55 | 1985 | 1407 | 100 | 670 | 520 |
| 60 | 2135 | 1628 |  |  |  |

## Notes:

1. PSD values are from Section 28-2.
2. $K=\frac{P S D^{2}}{2800}$, where : $h_{1}=3.5 \mathrm{ft}, h_{2}=3.5 \mathrm{ft}$
3. $K=\frac{P S D^{2}}{864}$, where : $h_{1}=1.080 \mathrm{~m}, h_{2}=1.080 \mathrm{~m}$

## K-VALUES FOR CREST VERTICAL CURVES - PASSING SIGHT DISTANCES (Passenger Cars)

Figure 30-2C

## 30-2.02 Sag Vertical Curves

## 30-2.02(a) Basic Equations

Sag vertical curves are in the shape of a parabola. Typically, they are designed to allow the vehicular headlights to illuminate the roadway surface (i.e., the height of object $=0.0 \mathrm{ft}(\mathrm{m})$ ) for a given distance " S ." The light beam from the headlights is assumed to have a $1^{\circ}$ upward divergence from the longitudinal axis of the vehicle. These assumptions yield the following basic equations for determining the minimum length of sag vertical curves:

$$
\begin{align*}
& \mathrm{L}=\frac{\mathrm{AS}^{2}}{200\left[\mathrm{~h}_{3}+\mathrm{S}\left(\tan 1^{\circ}\right)\right]}=\frac{\mathrm{AS}^{2}}{200 \mathrm{~h}_{3}+3.5 \mathrm{~S}}  \tag{Equation30-2.4}\\
& \mathrm{~L}=\mathrm{KA} \tag{Equation30-2.2}
\end{align*}
$$

Where:
$\mathrm{L} \quad=$ length of vertical curve, $\mathrm{ft}(\mathrm{m})$
A = algebraic difference between the two tangent grades, \%
$\mathrm{S}=$ sight distance, $\mathrm{ft}(\mathrm{m})$
$\mathrm{h}_{3}=$ height of headlights above pavement surface, $\mathrm{ft}(\mathrm{m})$
$\mathrm{K}=$ horizontal distance needed to produce a $1.0 \%$ change in gradient
The length of a sag vertical curve will depend upon "A" for the specific curve and upon the selected sight distance and headlight height. For design purposes, round the calculated length to the next highest $10 \mathrm{ft}(10 \mathrm{~m})$ increment.

## 30-2.02(b) Curve Lengths

The following discusses the application of K-values:

1. Vertical Point of Intersection (VPI). For sag vertical curves, it is acceptable to use an angle point (i.e., no vertical curve) up to an algebraic difference of grade ( $\Delta$ ) of $0.6 \%$ or less.
2. Stopping Sight Distance (SSD). The principal control in the design of sag vertical curves is to ensure that SSD is available for headlight illumination throughout the sag vertical curve. Figures $30-2 \mathrm{D}$ and $30-2 \mathrm{E}$ present K -values for passenger cars assuming $\mathrm{h}_{3}=2.0$ $\mathrm{ft}(600 \mathrm{~mm})$ and $\mathrm{S}=\mathrm{SSD}$ in the basic equation for sag vertical curves (Equation 30-2.4). These values represent the lowest acceptable sight distance on a facility. However, the designer should strive to use longer than the minimum lengths of curves to provide a more aesthetically pleasing design.

## BUREAU OF LOCAL ROADS \& STREETS

August 2016

| US Customary |  |  |  | Metric |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Design <br> Speed <br> $(\mathrm{mph})$ | Rate of <br> SSD(1) <br> $(\mathrm{ft})$ | Certical <br> Curvature, <br> K(2)(3) <br> $(\mathrm{ft} / \%)$ | Minimum <br> Curve <br> Length (ft) | Design <br> Speed <br> $(\mathrm{km} / \mathrm{h})$ | Rate of <br> Vertical <br> SSD(1) <br> $(\mathrm{m})$ | Curvature, <br> K(2)(4) <br> $(\mathrm{m} / \%)$ | Minimum <br> Curve <br> Length (m) |
| 20 | 115 | 17 | 60 | 30 | 35 | 6 | 18 |
| 25 | 155 | 26 | 75 | 40 | 50 | 9 | 24 |
| 30 | 200 | 37 | 90 | 50 | 65 | 13 | 30 |
| 35 | 250 | 49 | 105 | 60 | 85 | 18 | 36 |
| 40 | 305 | 64 | 120 | 70 | 105 | 23 | 42 |
| 45 | 360 | 79 | 135 | 80 | 130 | 30 | 48 |
| 50 | 425 | 96 | 150 | 90 | 160 | 38 | 54 |
| 55 | 495 | 115 | 165 | 100 | 185 | 45 | 60 |
| 60 | 570 | 136 | 180 |  |  |  |  |

## Notes:

1. SSD values are from Figure 28-1A.
2. Maximum K-value for drainage on curbed roadways and bridges is 167 (51).
3. $K=\frac{S S D^{2}}{400+3.5 S S D}$, where : $h_{3}=2 \mathrm{ft}$
4. 



K-VALUES FOR SAG VERTICAL CURVES — STOPPING SIGHT DISTANCES (Passenger Cars)

Figure 30-2D



DESIGN CONTROLS FOR SAG VERTICAL CURVES
Figure 30-2E

## HARD COPIES UNCONTROLLED

3. Minimum Length. For most sag vertical curves, the minimum length of curve should also be based on the following equations:
$L_{\text {min }}=3 \mathrm{~V}$
(US Customary) Equation 30-2.3
$\mathrm{L}_{\text {min }}=0.6 \mathrm{~V}$
(Metric) Equation 30-2.3
Where:

$$
\begin{aligned}
\mathrm{L}_{\text {min }} & =\text { minimum length of vertical curve, } \mathrm{ft}(\mathrm{~m}) \\
\mathrm{V} & =\text { design speed, } \mathrm{mph}(\mathrm{~km} / \mathrm{h})
\end{aligned}
$$

Designs with vertical curve lengths of less than $90 \mathrm{ft}(27 \mathrm{~m})$ should be avoided, since these are difficult to construct.
4. Comfort Criteria. On fully lighted, continuous sections of highway and where it is impractical to provide SSD for headlights, a sag vertical curve may be designed to meet the comfort criteria. The length of curve equation for the comfort criteria is:

$$
\mathrm{L}=\frac{\mathrm{AV}^{2}}{46.5}
$$

(US Customary) Equation 30-2.5

$$
\mathrm{L}=\frac{\mathrm{AV}^{2}}{395}
$$

(Metric) Equation 30-2.5
Where:

$$
\begin{aligned}
\mathrm{L} & =\text { length of vertical curve, } \mathrm{ft}(\mathrm{~m}) \\
\mathrm{A} & =\text { algebraic difference between the two tangent grades, } \% \\
\mathrm{~V} & =\text { design speed, } \mathrm{mph}(\mathrm{~km} / \mathrm{h})
\end{aligned}
$$

5. Drainage. Proper drainage must be considered in the design of sag vertical curves on curbed sections and bridges. Drainage problems are minimized if the sag vertical curve is sharp enough so that a minimum longitudinal grade of at least $0.3 \%$ is reached at a point about $50 \mathrm{ft}(15 \mathrm{~m})$ from either side of the low point. To ensure that this objective is achieved, base the length of the vertical curve upon a K-value of 167 (51) or less. This K-value is adequate for design speeds of $60 \mathrm{mph}(100 \mathrm{~km} / \mathrm{h})$ or less.

For uncurbed sections of highway, drainage should not be a problem at sag vertical curves.

## 30-3 VERTICAL CLEARANCES

The tables in Section 33-3 provide the roadway vertical clearances for $3 R$ projects on nonfreeways. The tables in Sections 36-4 and 36-5 present the minimum roadway vertical clearances for new construction and reconstruction projects. In addition to the criteria presented in Chapter 36, consider the following:

1. Existing Structures. The minimum clearance for structures allowed to remain-in-place is $14 \mathrm{ft}-0$ in $(4.3 \mathrm{~m})$ for all functional classifications.
2. Pedestrian Bridges/Sign Trusses. On all new or reconstruction projects, provide a minimum vertical clearance of $17 \mathrm{ft}-3$ in ( 5.25 m ) under pedestrian bridges and sign trusses. For 3 R projects existing pedestrian bridges and sign structures allowed to remain-in-place shall have a minimum clearance of $16 \mathrm{ft}-9 \mathrm{in}(5.1 \mathrm{~m})$.
3. Traffic Signals. On all new or reconstruction projects, provide a minimum vertical clearance of $16 \mathrm{ft}-0 \mathrm{in}(4.9 \mathrm{~m})$ with a maximum clearance of $18 \mathrm{ft}-0 \mathrm{in}(5.5 \mathrm{~m})$. For 3R projects, a minimum vertical clearance of $14 \mathrm{ft}-9 \mathrm{in}(4.5 \mathrm{~m})$ may be allowed to remain in place. This clearance is measured from the roadway surface to the bottom of the signal housing or to the bottom of the back plate.
4. Railroads. For all projects, the minimum vertical clearance for new and reconstructed structures over railroads is $23 \mathrm{ft}-0$ in $(7.0 \mathrm{~m})$ measured from the top of the highest rail. This clearance may be reduced with approval of the railroad and the Illinois Commerce Commission (ICC) (Title 92 Illinois Administrative Code, Part 1500, Chapter 3, Subpart C).

## 30-4 ACRONYMS

This is a summary of the acronyms used within this chapter.

| 3R | Rehabilitation, Restoration, and/or Resurfacing |
| :--- | :--- |
| AASHTO | American Association of State Highway and Transportation Officials |
| BDE | Bureau of Design and Environment |
| CBLRS | Central Bureau of Local Roads and Streets |
| ICC | Illinois Commerce Commission |
| IDOT | Illinois Department of Transportation |
| PSD | Passing Sight Distance |
| PVI | Point of Vertical Intersection |
| SSD | Stopping Sight Distance |

## 30-5 REFERENCES

1. A Policy on Geometric Design of Highways and Streets, AASHTO, 2011.
2. NCHRP Report 400, Determination of Stopping Sight Distances, Transportation Research Board, 1997.
3. IDOT Drainage Manual, Illinois Department of Transportation.
4. Chapter 33 "Vertical Alignment," Bureau of Design and Environment Manual, IDOT.
